



Applied Aerodynamics
Technical Committee

3rd CFD Drag Prediction Workshop

San Francisco, California – June 2006

Case 1 F6 Fairing Drag Prediction for the 3rd CFD Drag Prediction Workshop

Edward N. Tinoco

&

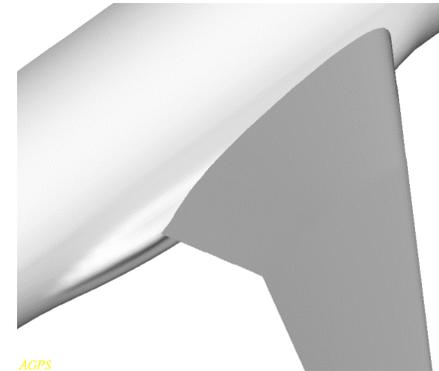
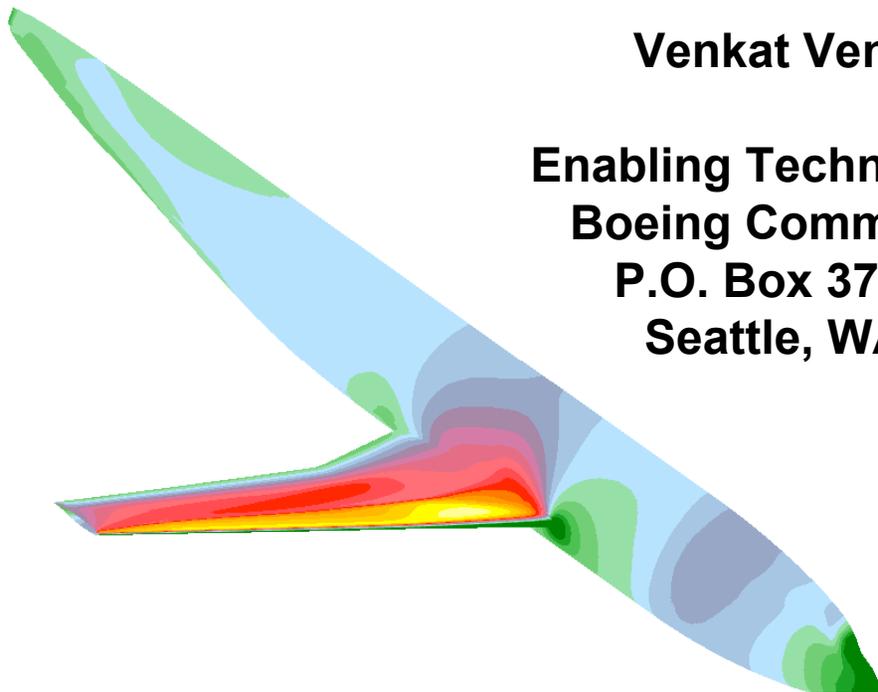
Venkat Venkatakrishnan

Enabling Technology & Research

Boeing Commercial Airplanes

P.O. Box 3707 MC 67-LK

Seattle, WA 98124-2207



AGPS



Objective

Investigate the use of a “Production Navier-Stokes Analysis System” for CFD Drag Prediction

-Major interest is in the prediction of drag increments

-Use “standard” processes as much as possible

Acknowledgement

None of this work would have been possible without the considerable contributions of:

N. Jong Yu

Tsu-Yi Bernard Su

Tsong-Jhy Kao

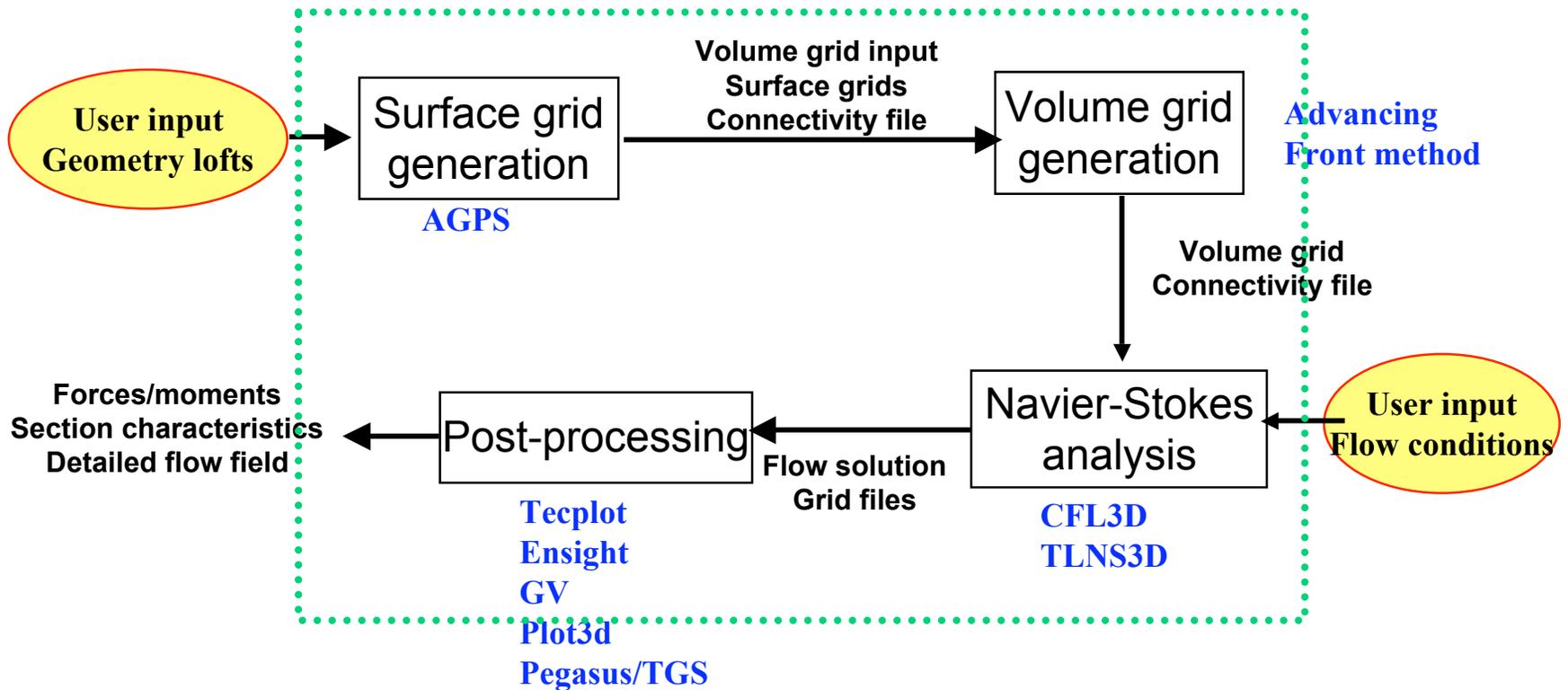
Senthan Swaminathan

Moeljo Hong

Emanuel R Setiawan

ZEUS/CFL3D

Driver for Surface Grid Generation, Volume Grid Generation,
Navier-Stokes Analysis, and Post-processing

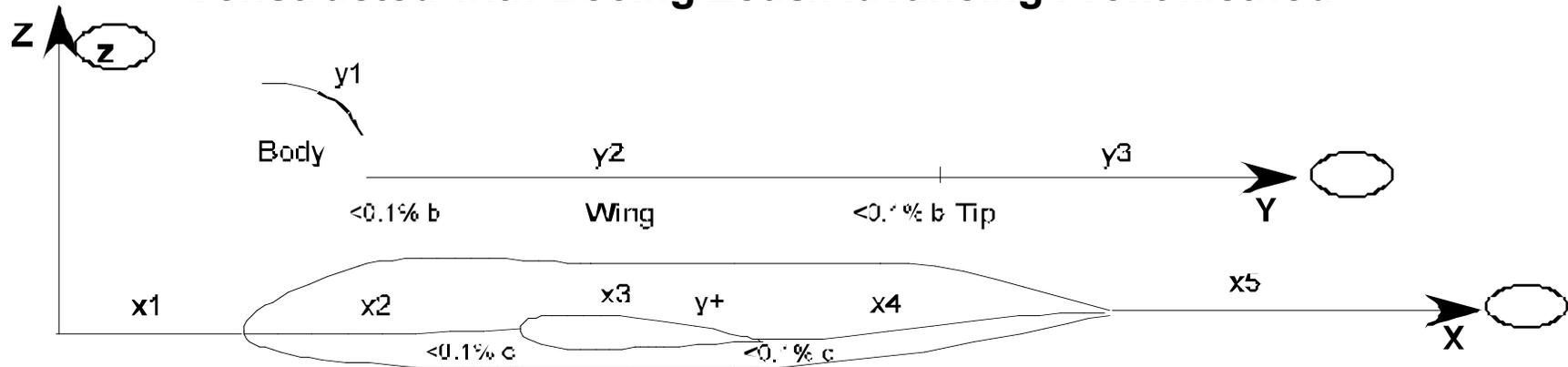




CFL3D – Thin Layer Navier-Stokes Code

- Developed at NASA Langley (Jim Thomas, Kyle Anderson, Bob Biedron, Chris Rumsey, & ...)
- Finite volume
- Upwind biased and central difference
- Multigrid and mesh sequencing for acceleration
- Multiblock with 1-1 blocking, patched grid, and overlap-grid
- Numerous turbulence models
 - Spalart-Almaras SA Model
 - Menter's $k-\omega$ SST Model
- Time accurate with dual-time stepping
- Runs efficiently on parallel machines through MPI

Structured Multi-Block Wing-Body Grids Constructed with Boeing Zeus/Advancing Front Method



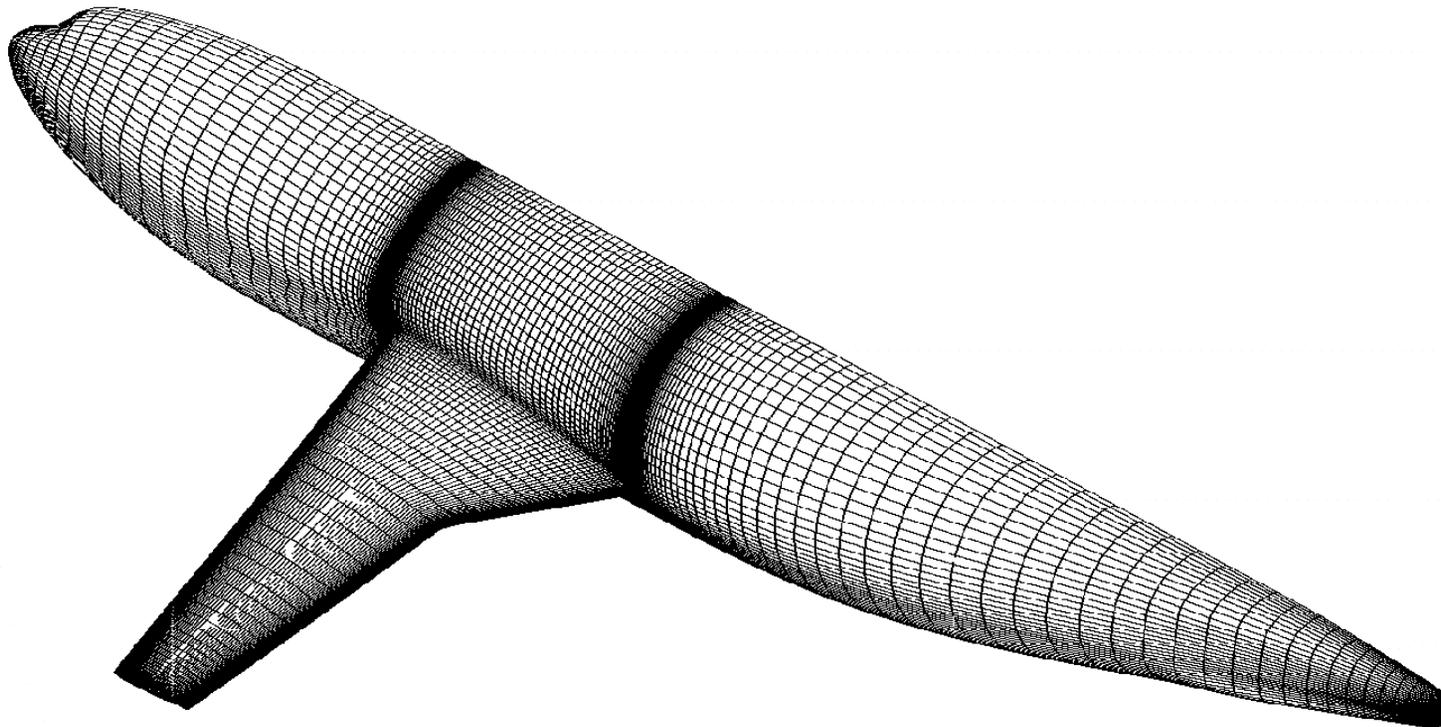
| | x1 | x2 | x3 | x4 | x5 | y1 | y2 | y3 | z |
|---------|----|-----|-----|-----|----|----|-----|----|-----|
| Course | 16 | 48 | 80 | 56 | 16 | 24 | 48 | 16 | 56 |
| Med | 24 | 72 | 120 | 88 | 24 | 32 | 72 | 24 | 84 |
| Medfine | 28 | 92 | 156 | 112 | 32 | 36 | 92 | 28 | 104 |
| Fine | 32 | 108 | 180 | 136 | 36 | 56 | 112 | 32 | 128 |

| Blunt TE | z | y2 |
|----------|----|-----|
| Course | 32 | 48 |
| Med | 48 | 72 |
| Medfine | 60 | 92 |
| Fine | 72 | 112 |

| Boundary Layer | # Cells | Ave y+ |
|----------------|---------|--------|
| Course | 24 | 0.82 |
| Med | 32 | 0.60 |
| Medfine | 40 | 0.50 |
| Fine | 48 | 0.40 |

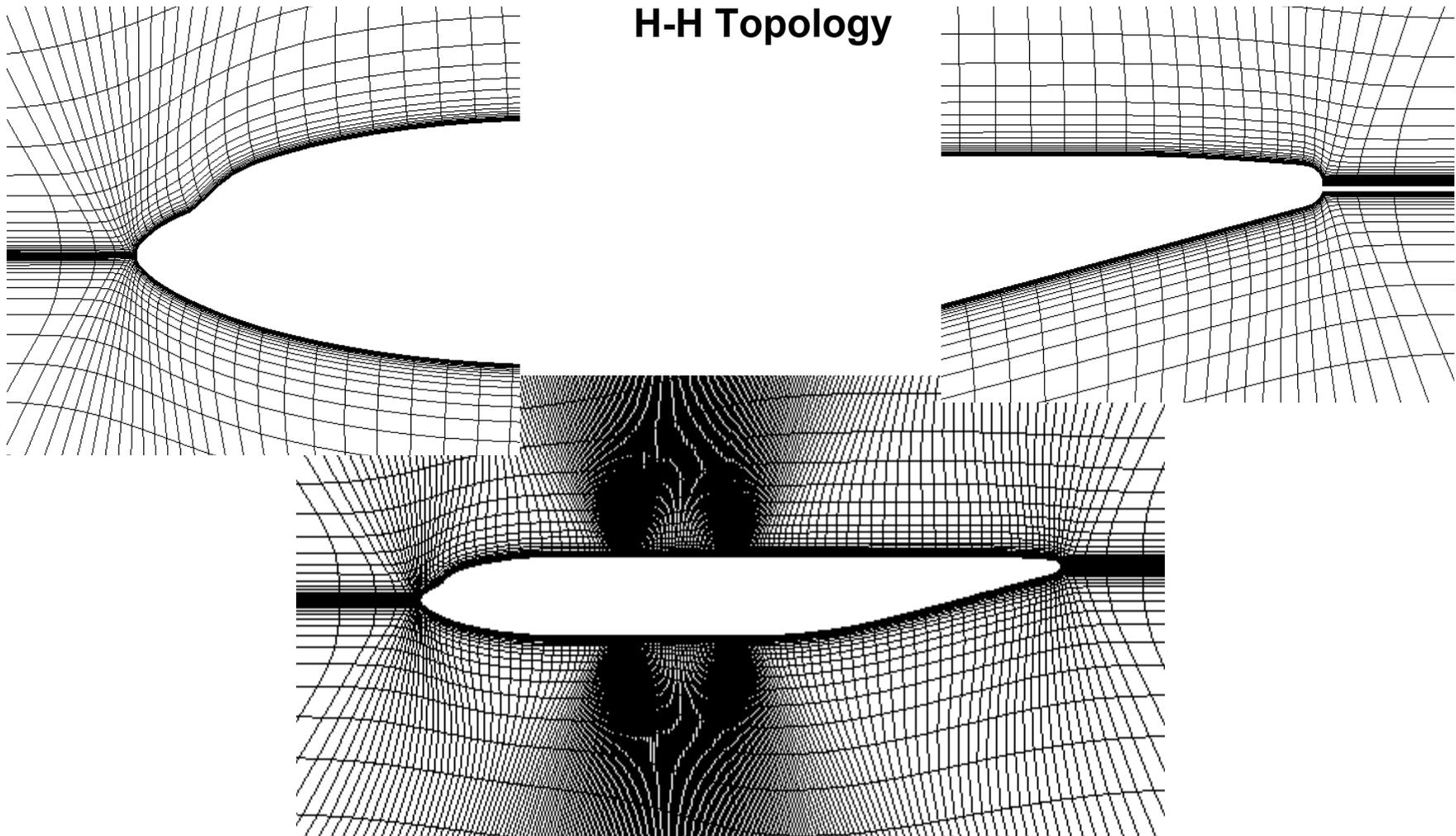
| Total Grid Size |
|-----------------|
| 2.6E+06 |
| 9.2E+06 |
| 1.8E+07 |
| 3.1E+07 |

Structured Multi-Block Wing-Body Grids Constructed with Boeing Zeus/Advancing Front Method

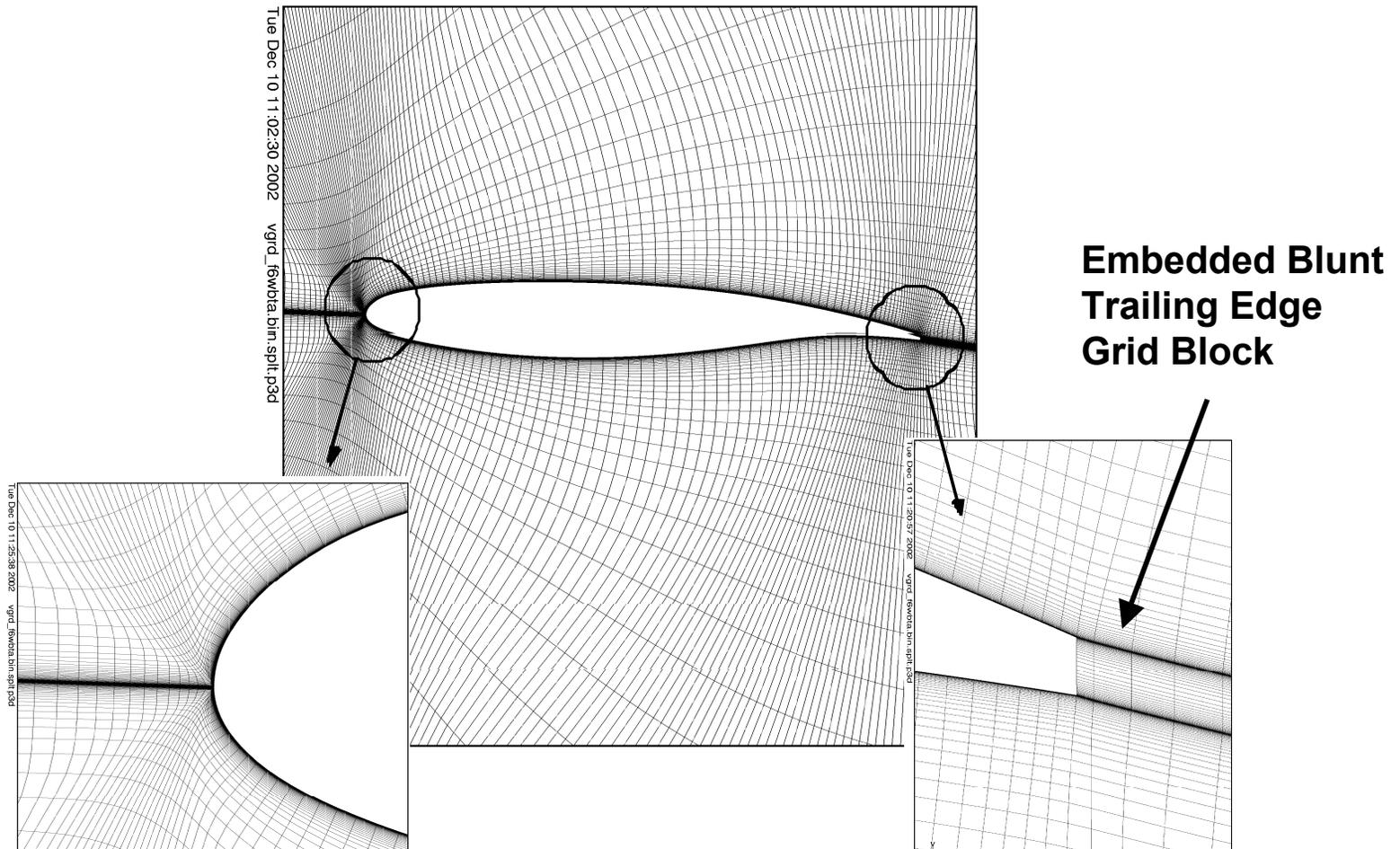


Typical Centerline Grid

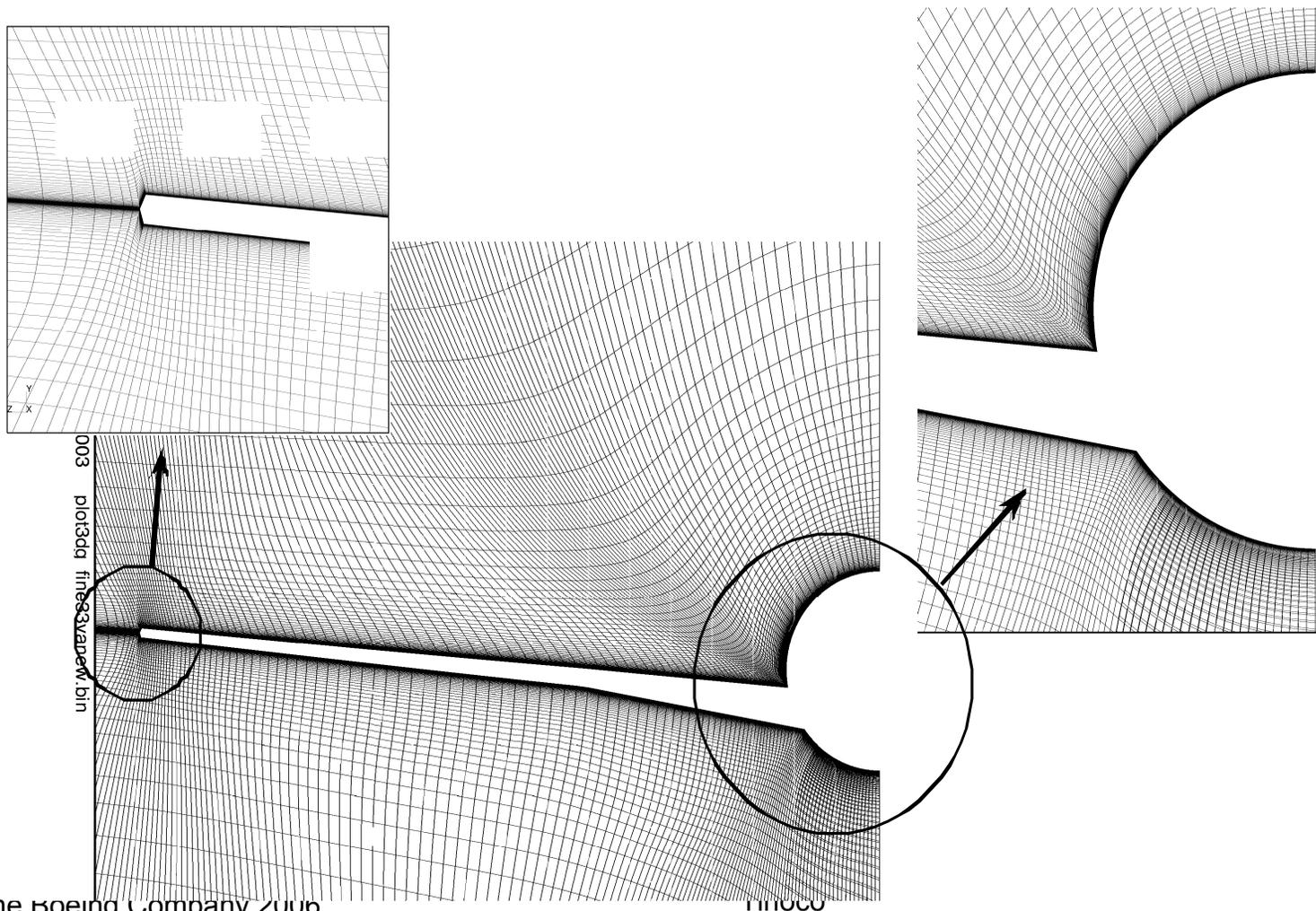
H-H Topology



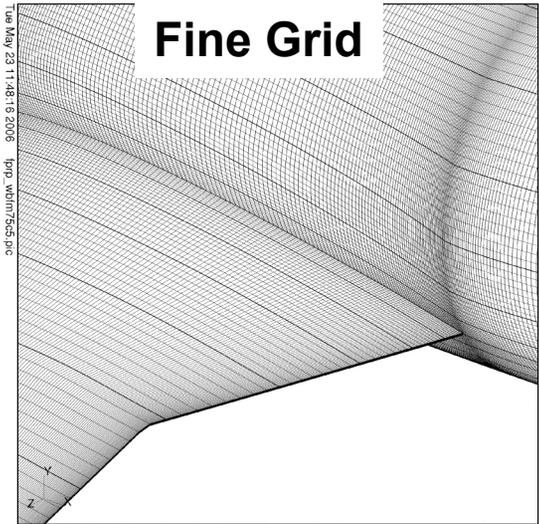
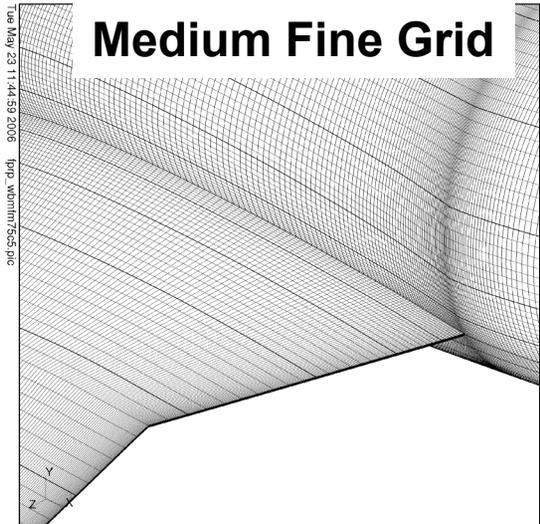
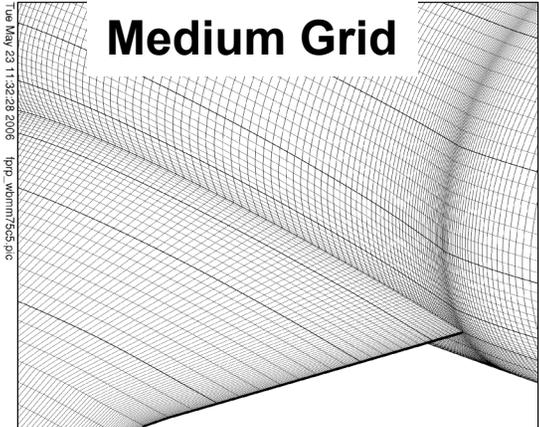
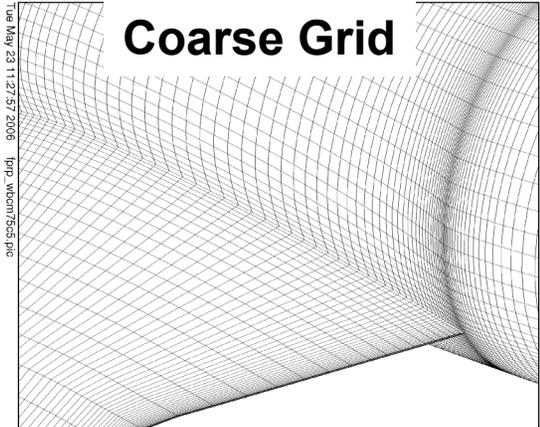
Typical Wing Grid H-H Topology



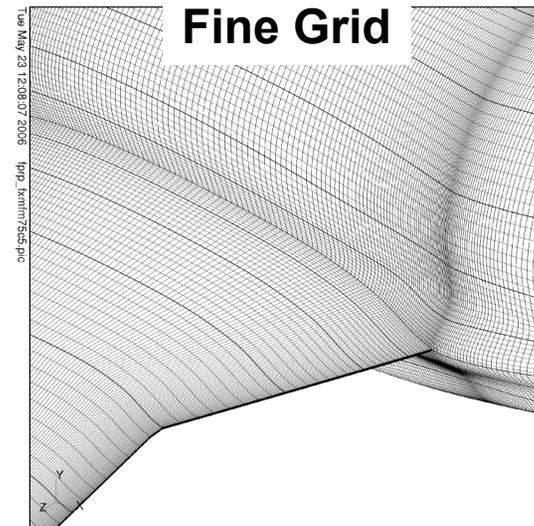
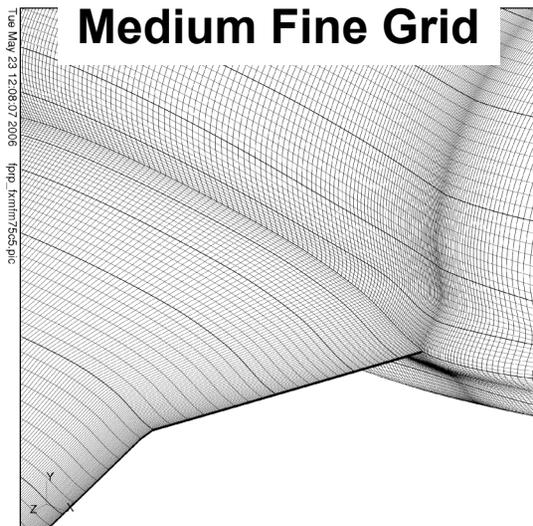
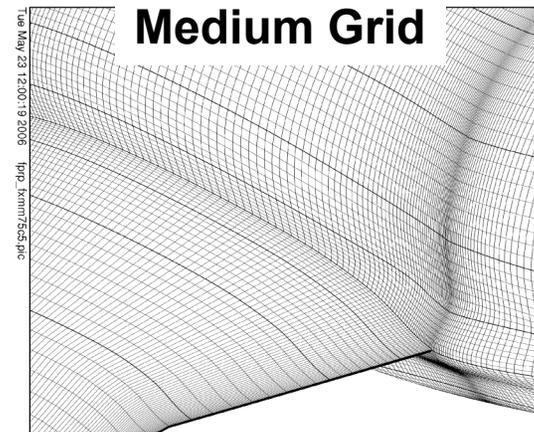
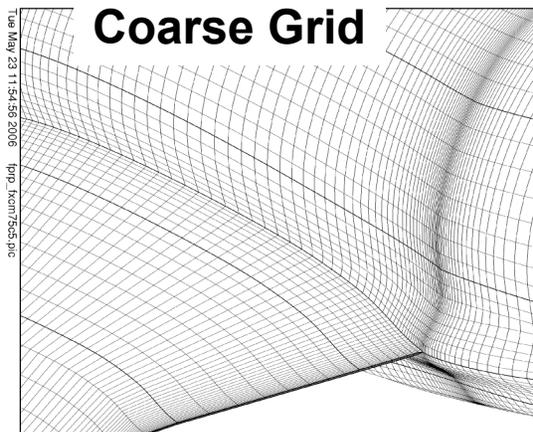
Typical I-plane Grid H-Topology



Grid Refinement – F6 Wing-Body

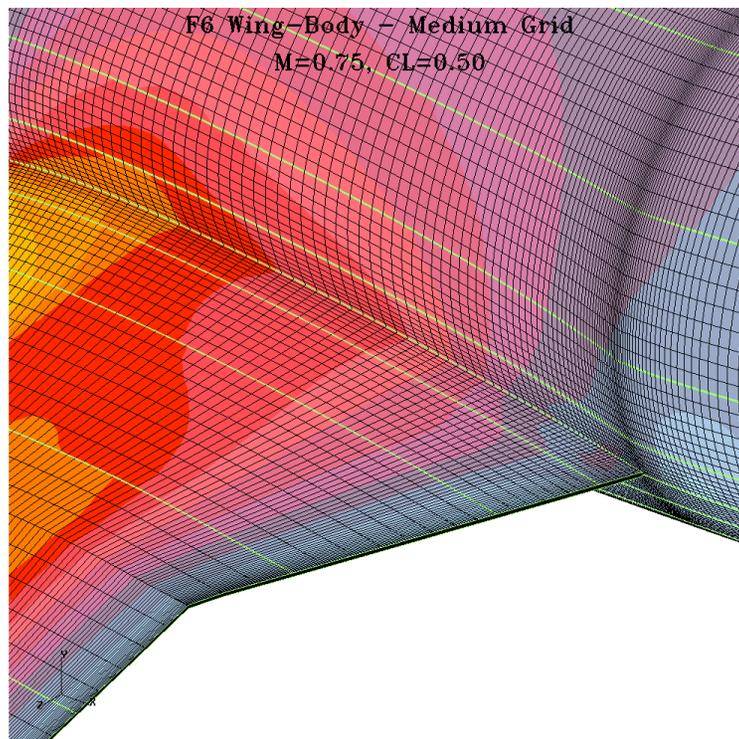


Grid Refinement – F6 Wing-Body w/FX2 Fairing

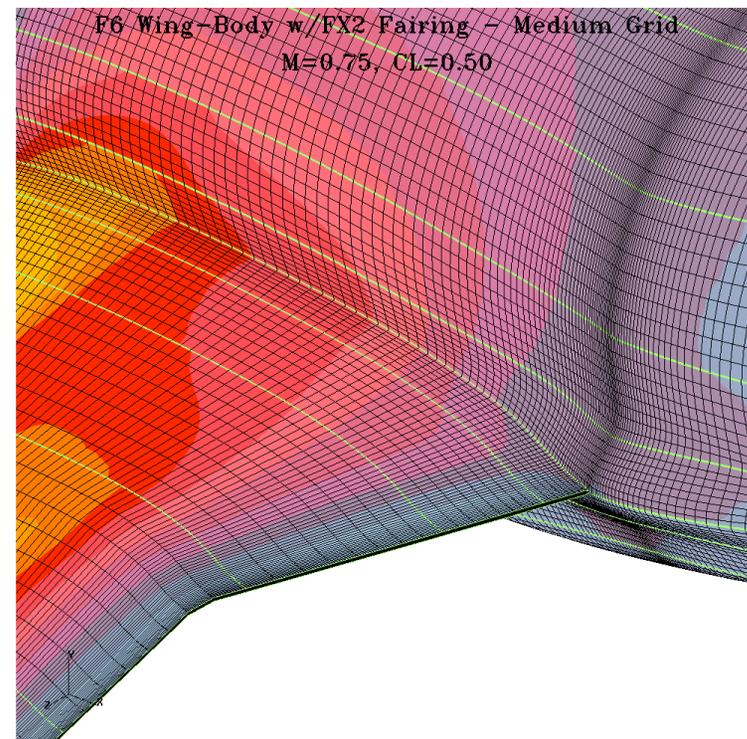


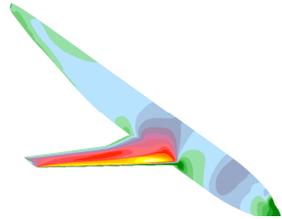
Medium Grid F6 Wing-Body w/wo/FX2 Fairing

F6 Wing-Body



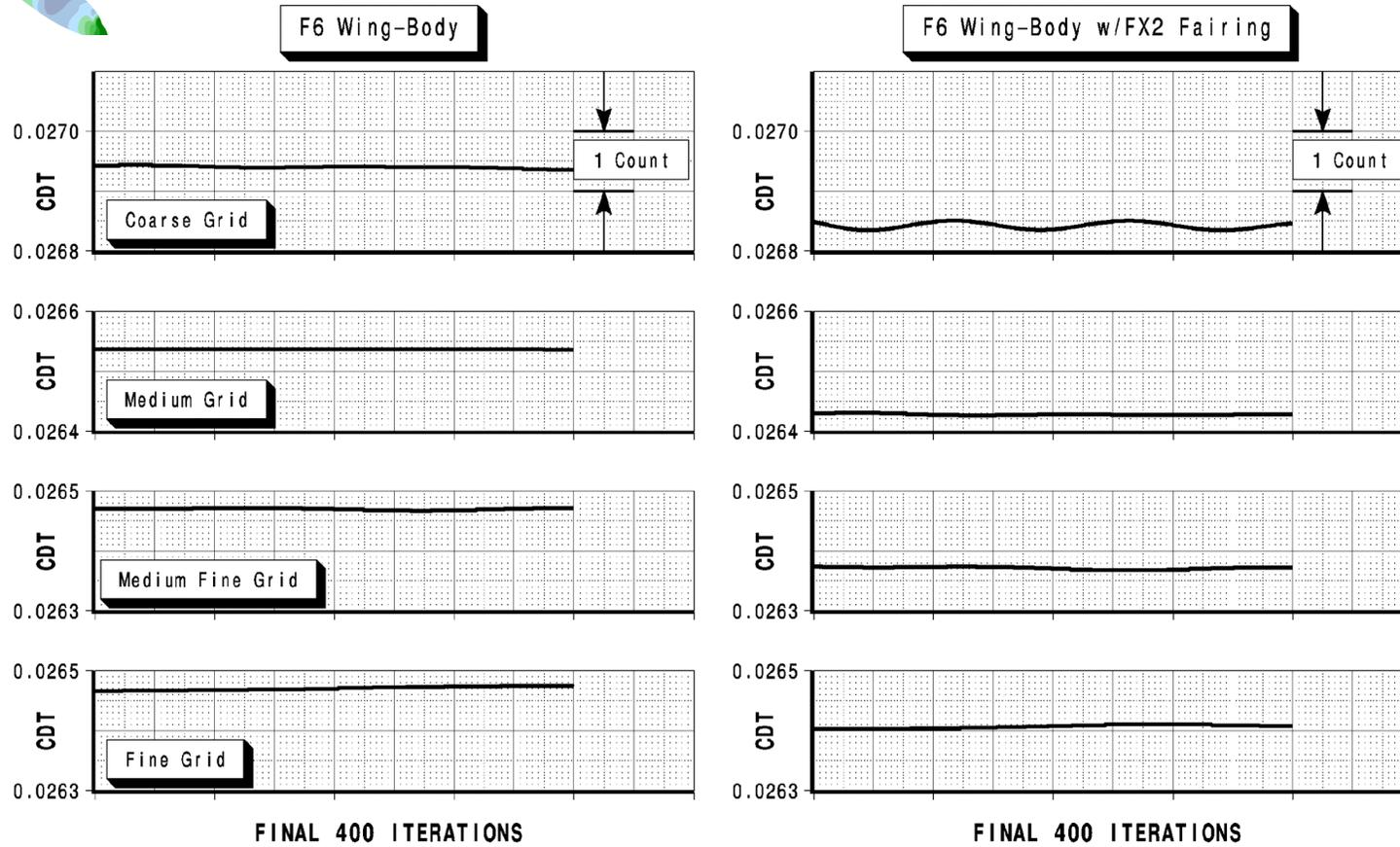
F6 Wing-Body w/FX2 Fairing



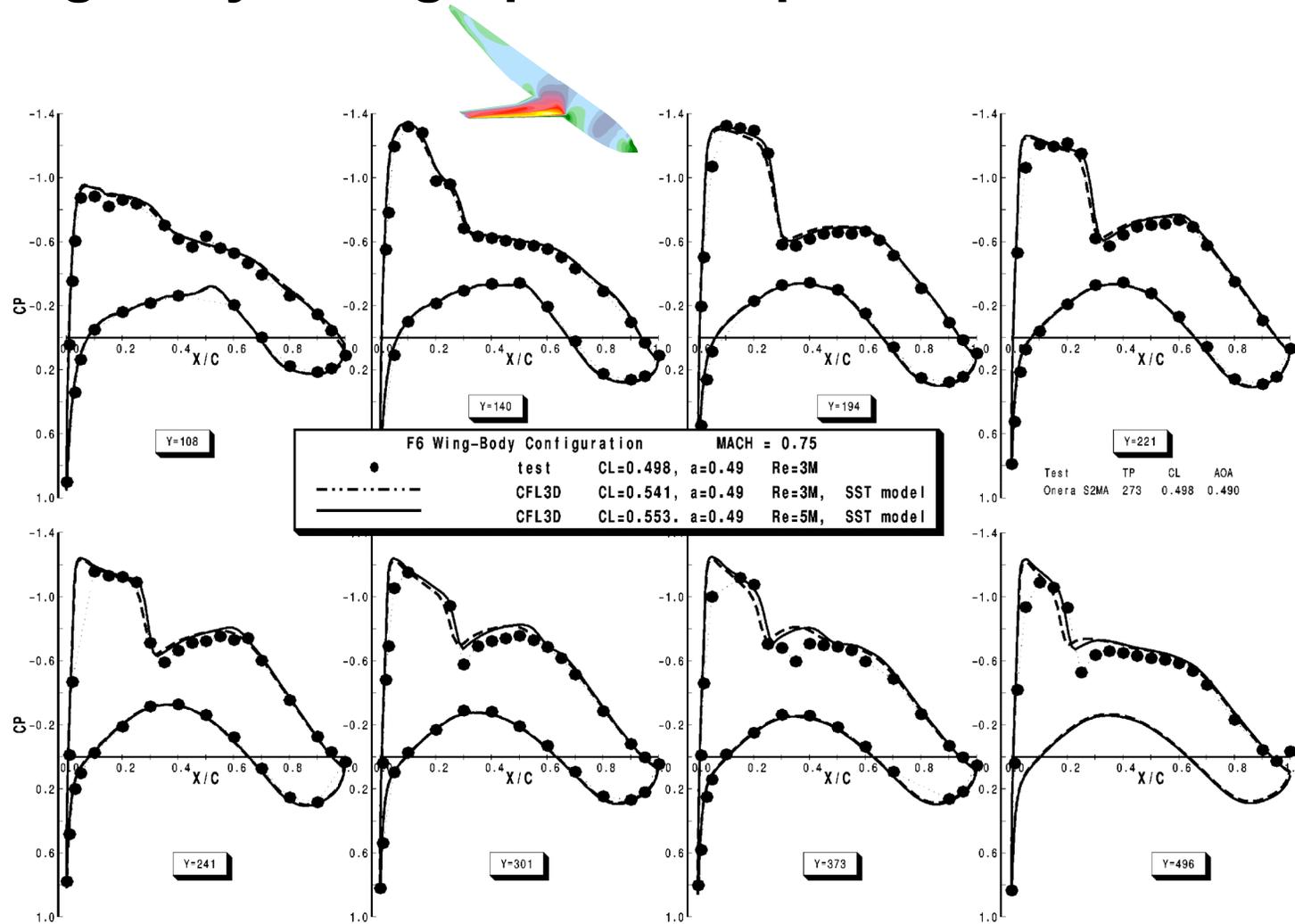


F6 WB w/wo FX2 – Drag Convergence

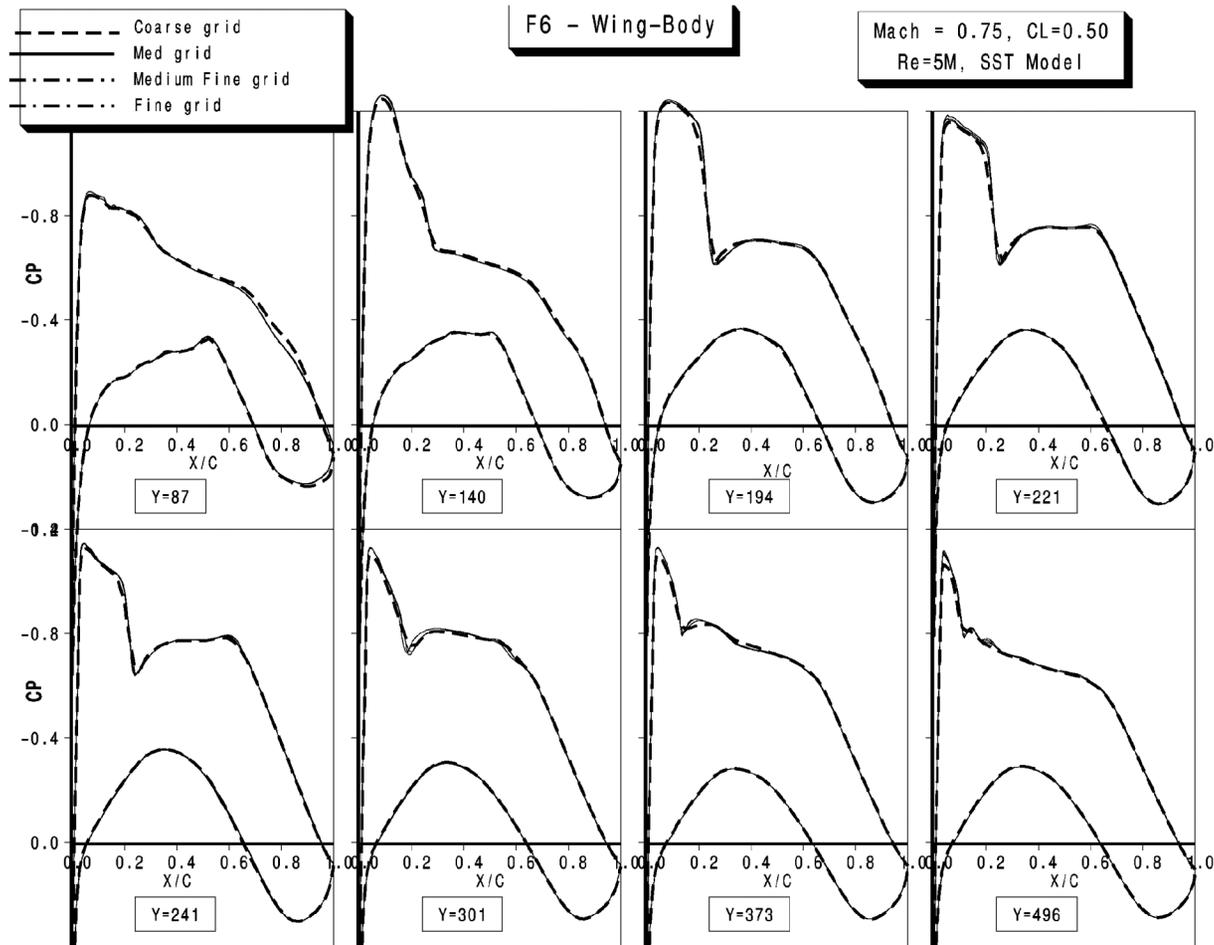
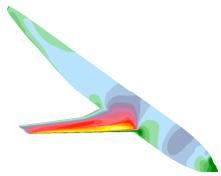
Mach=0.75, CL=0.50, Re=5M, SST Turbulence Model



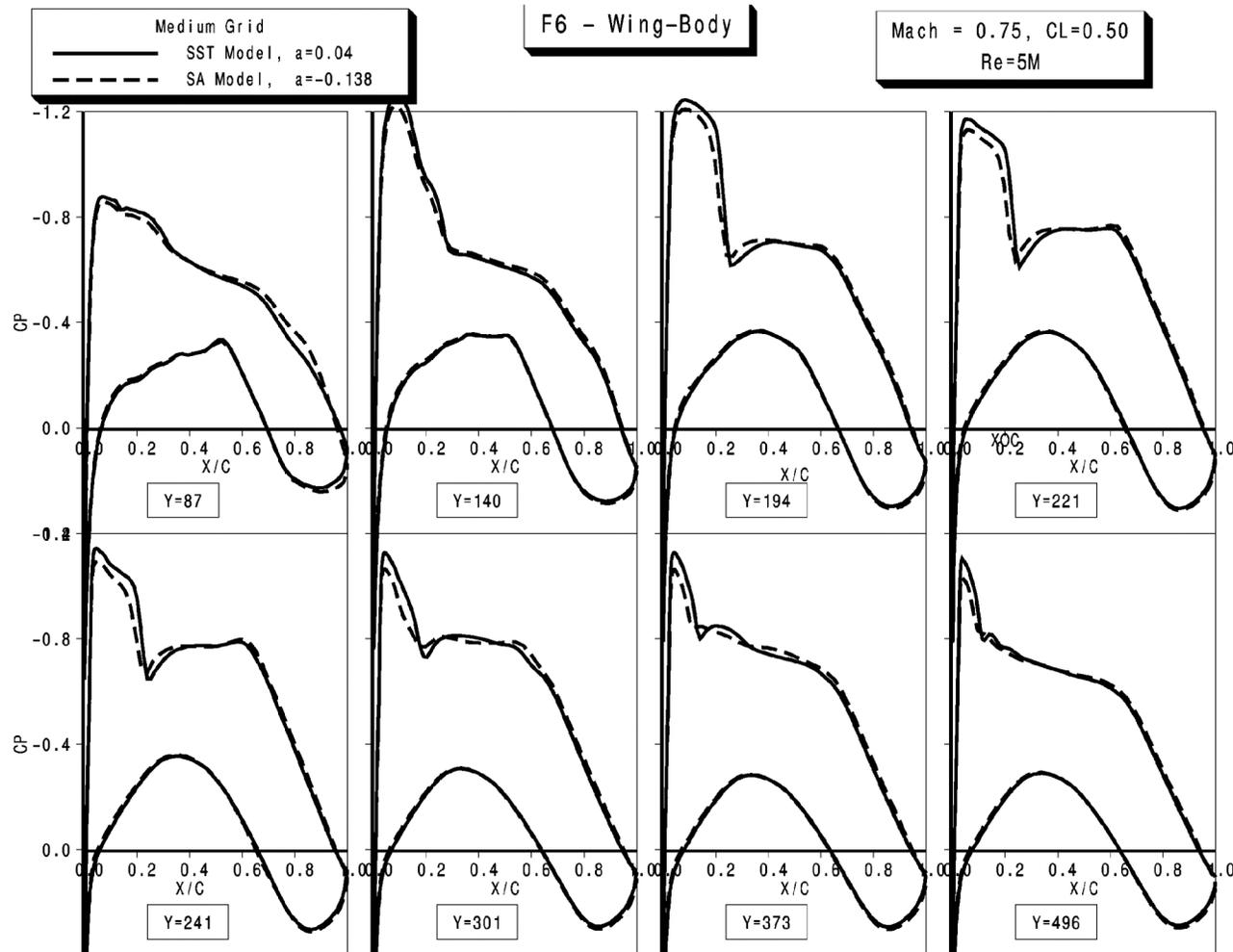
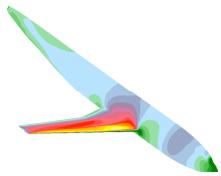
F6 Wing-Body - Wing Cp's – Comparison with Re=3M Test



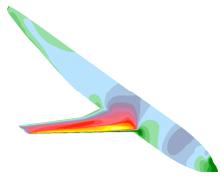
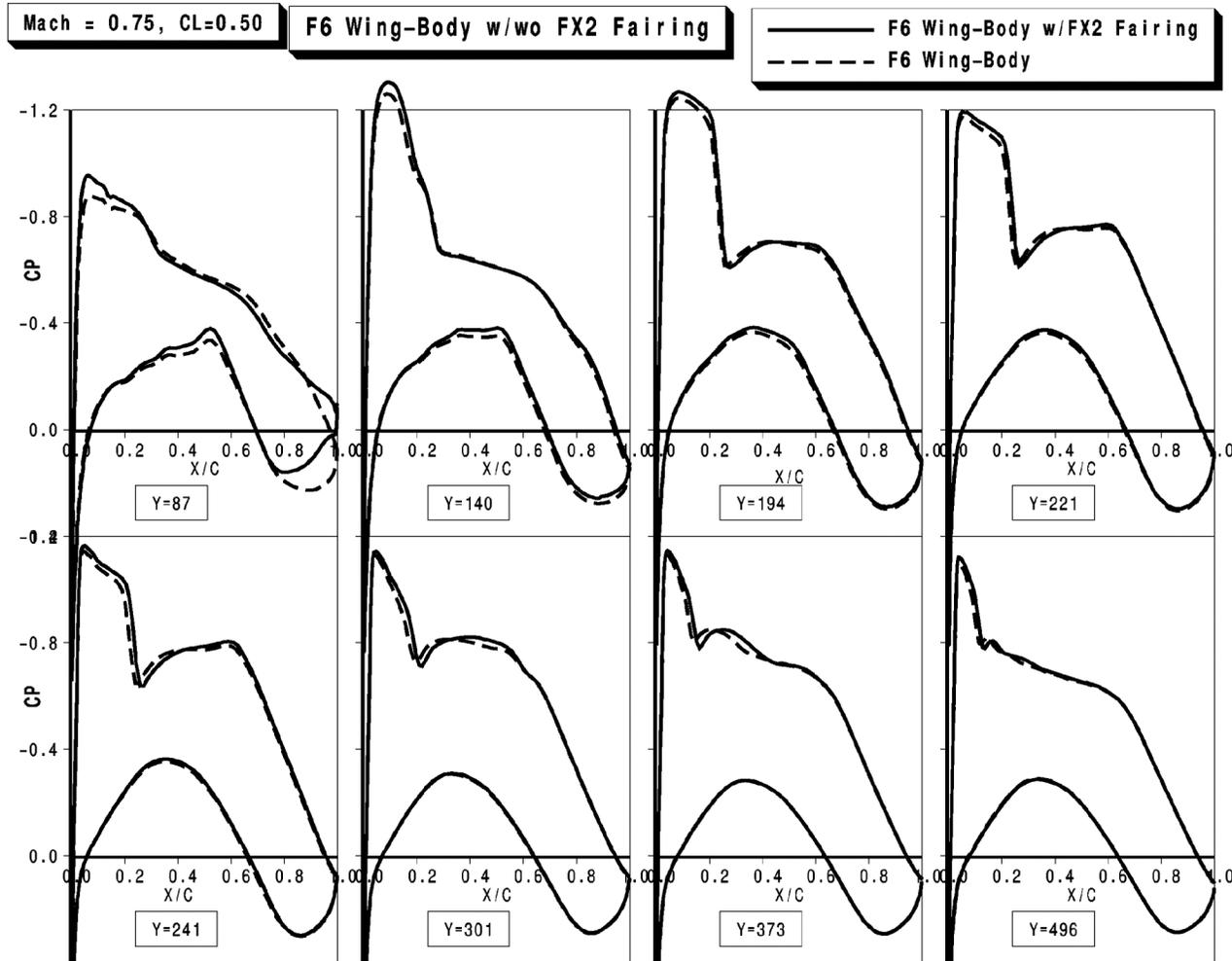
F6 Wing-Body - Wing Cp's – Grid Convergence



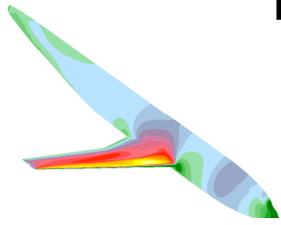
F6 Wing-Body - Wing C_p 's – Turbulence Modeling Effects



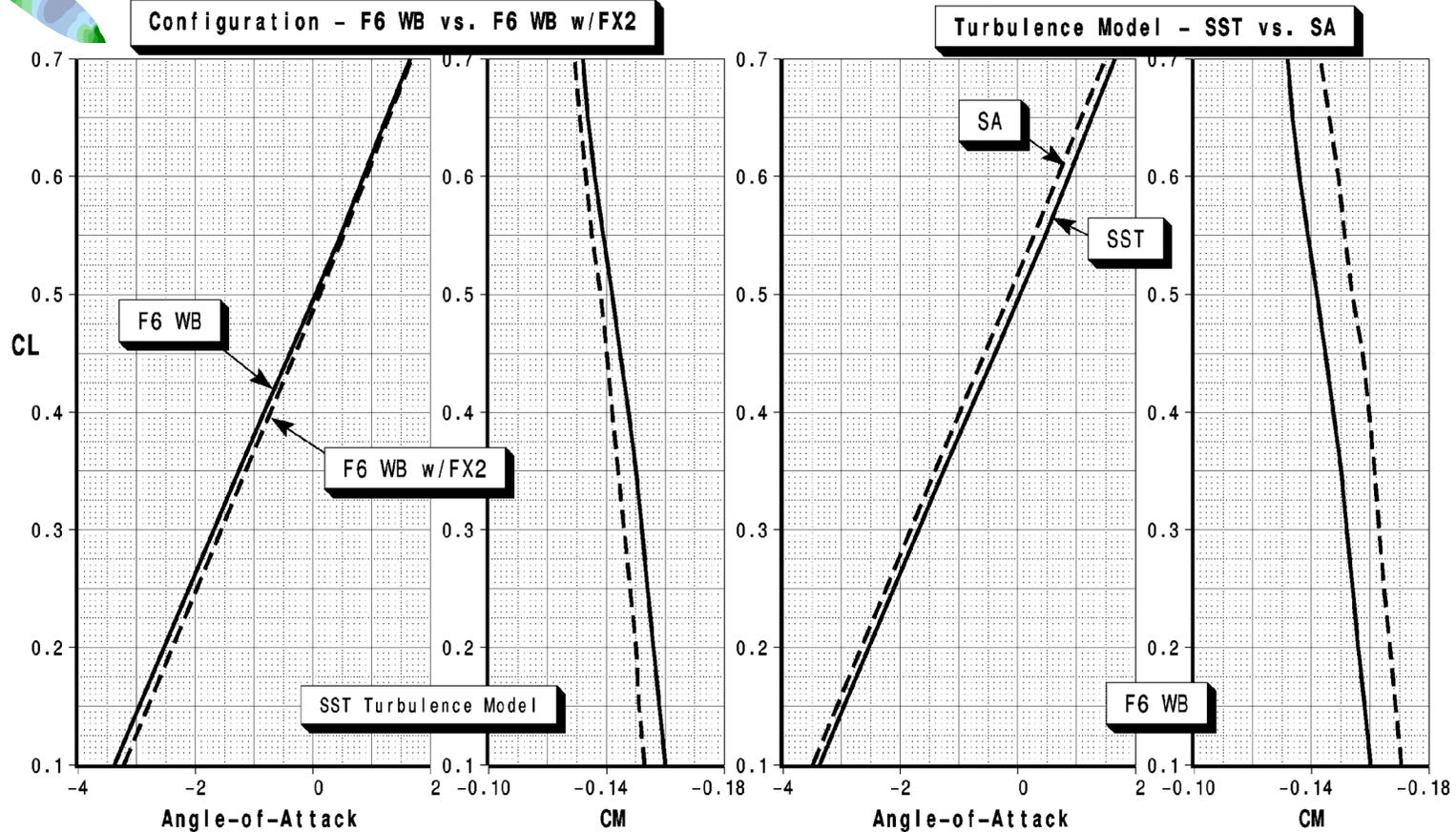
F6 Wing-Body - Wing Cp's – Effect of Fairing



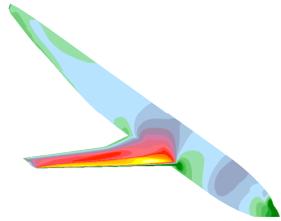
F6 WB w/wo FX2 – Lift and Pitching Moment



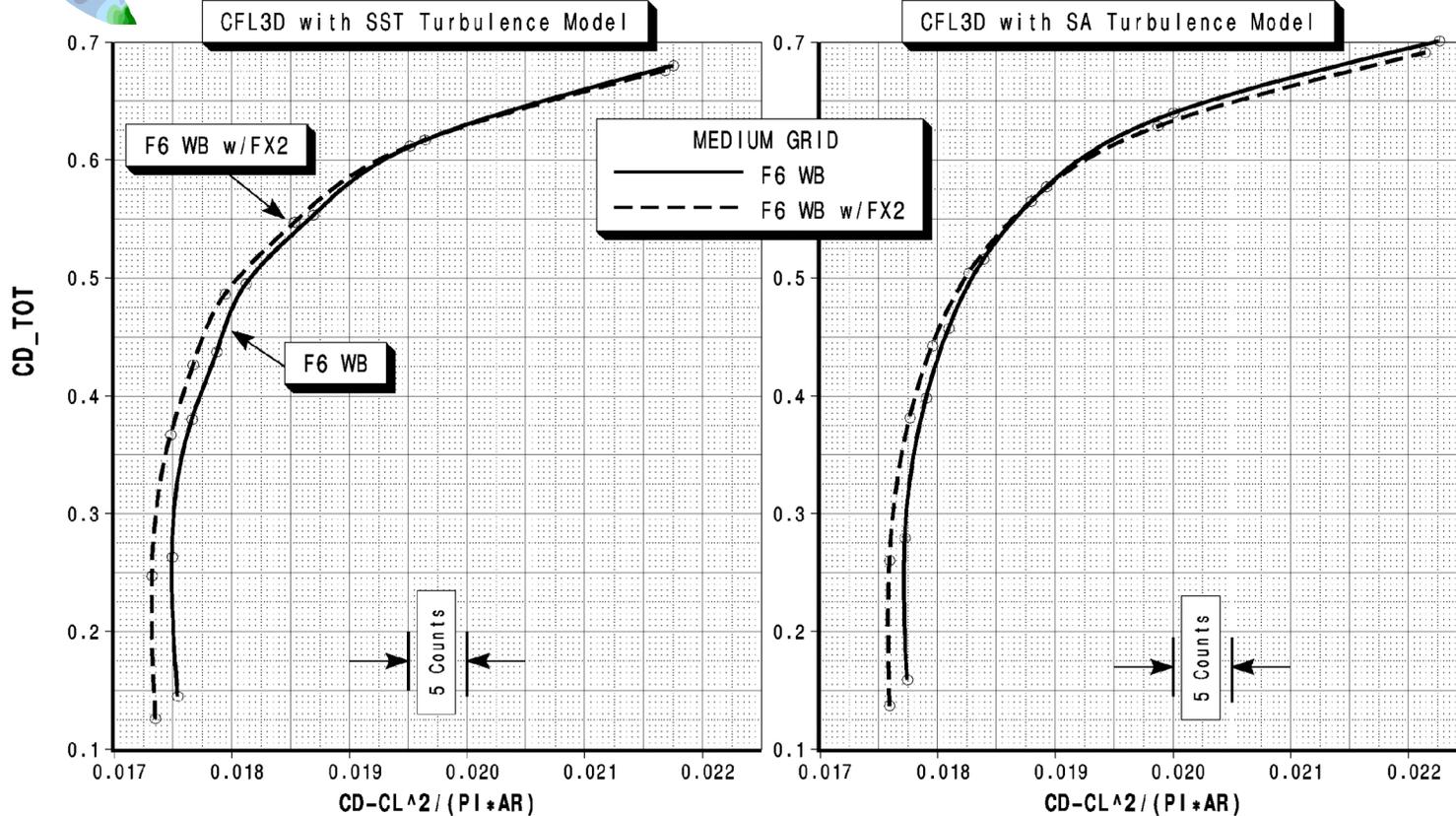
F6 WB w/wo FX2, MACH = 0.75
Re = 5 Million



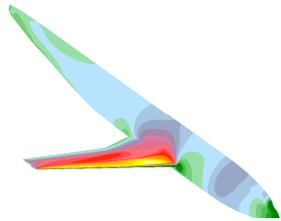
F6 WB w/wo FX2 - Polar Shape – Turbulence Modeling



F6 Wing-Body w/wo FX2, MACH = 0.75
Re = 5 Million, Fixed CL=0.50

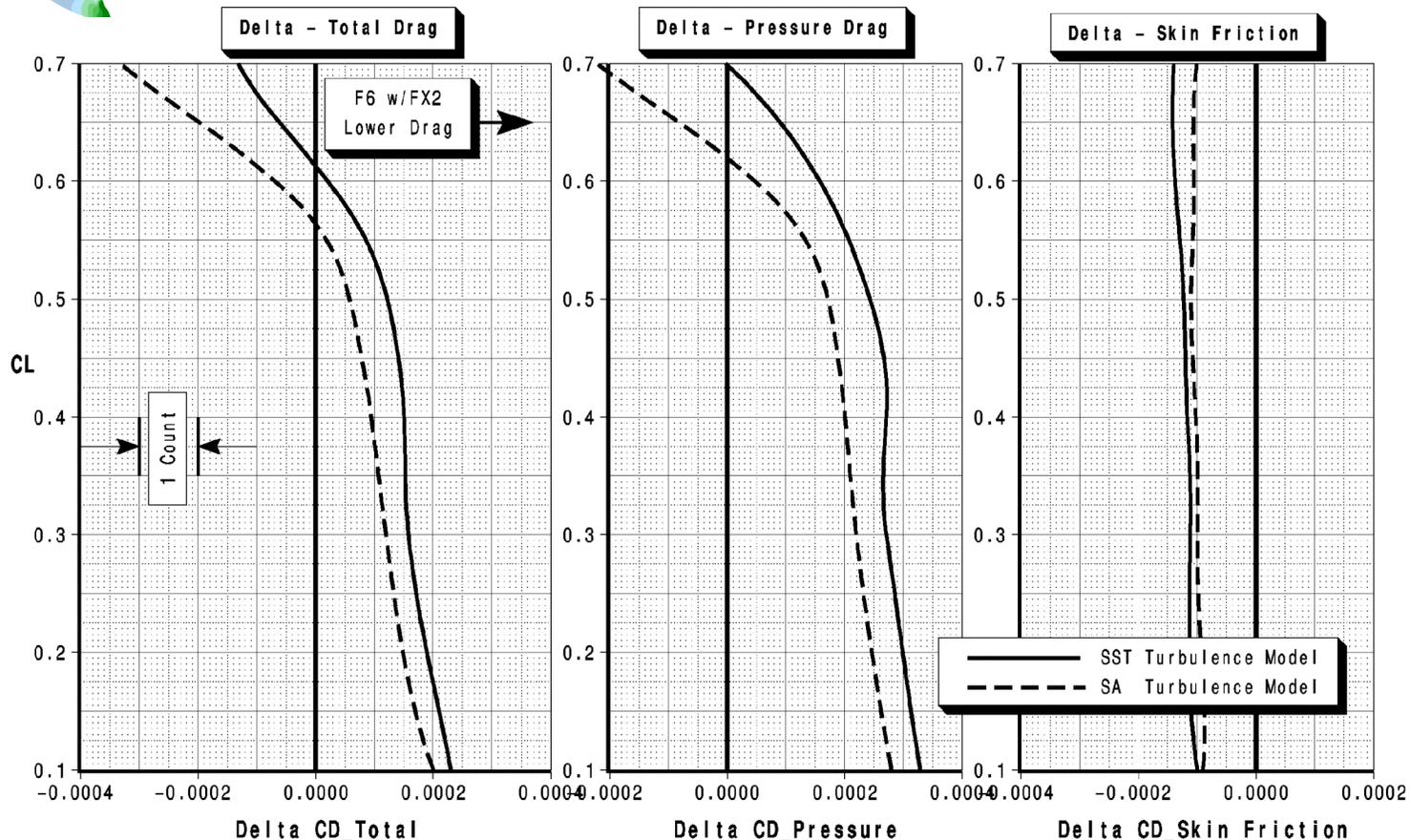


F6 WB w/wo FX2 – Drag Polar Increments

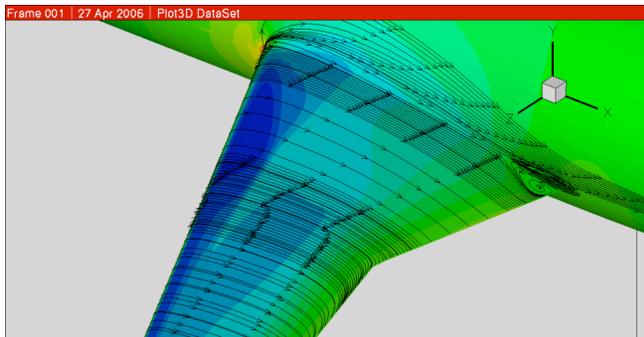


F6 Wing-Body w/wo FX2
MACH = 0.75, Re = 5 Million

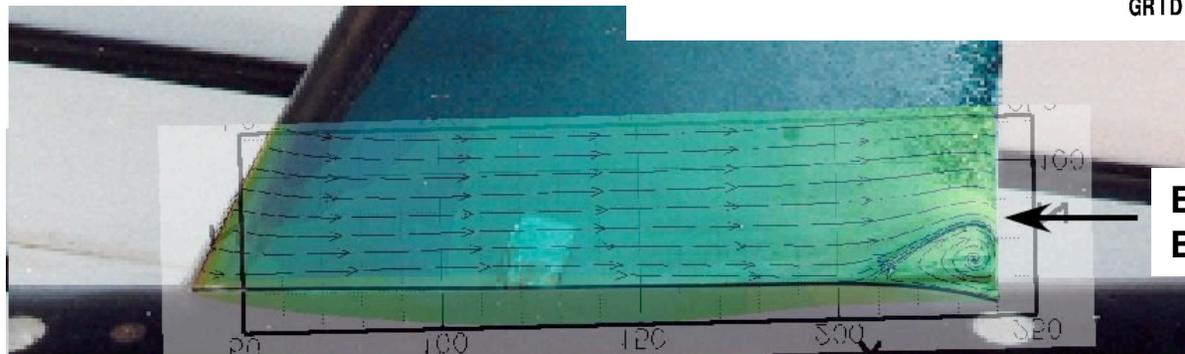
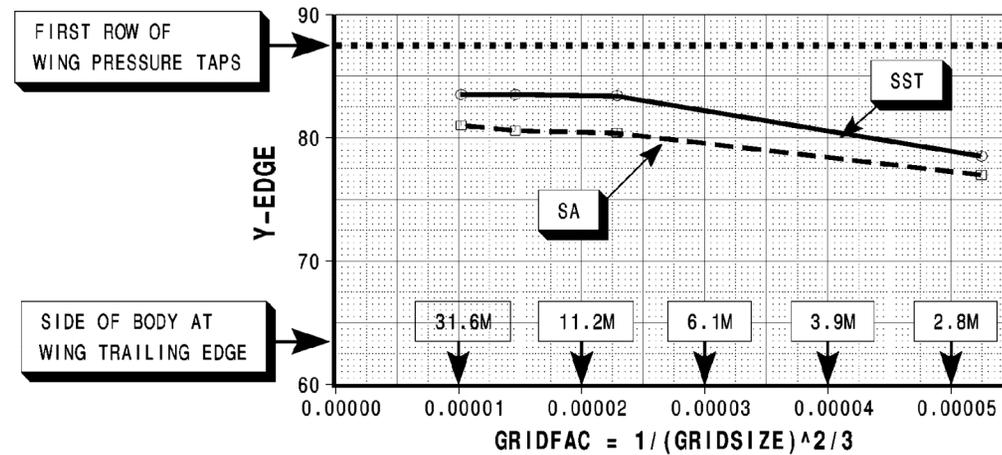
Delta CD (WB - WB w/FX2)



F6 WB Separation Bubble on Wing – Turbulence Modeling

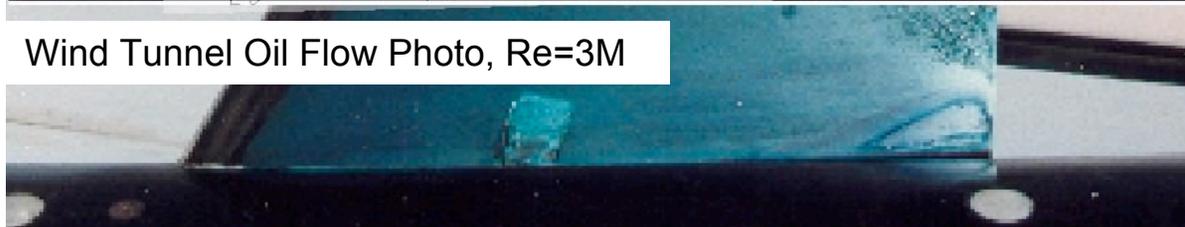


Overlay of Computed Streamlines,
SST Turbulence Model, Re=5M

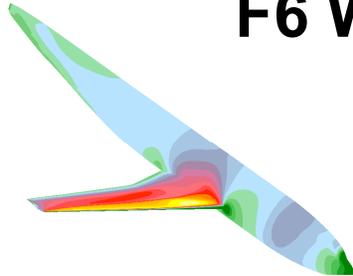


Edge of Separation
Bubble on Wing

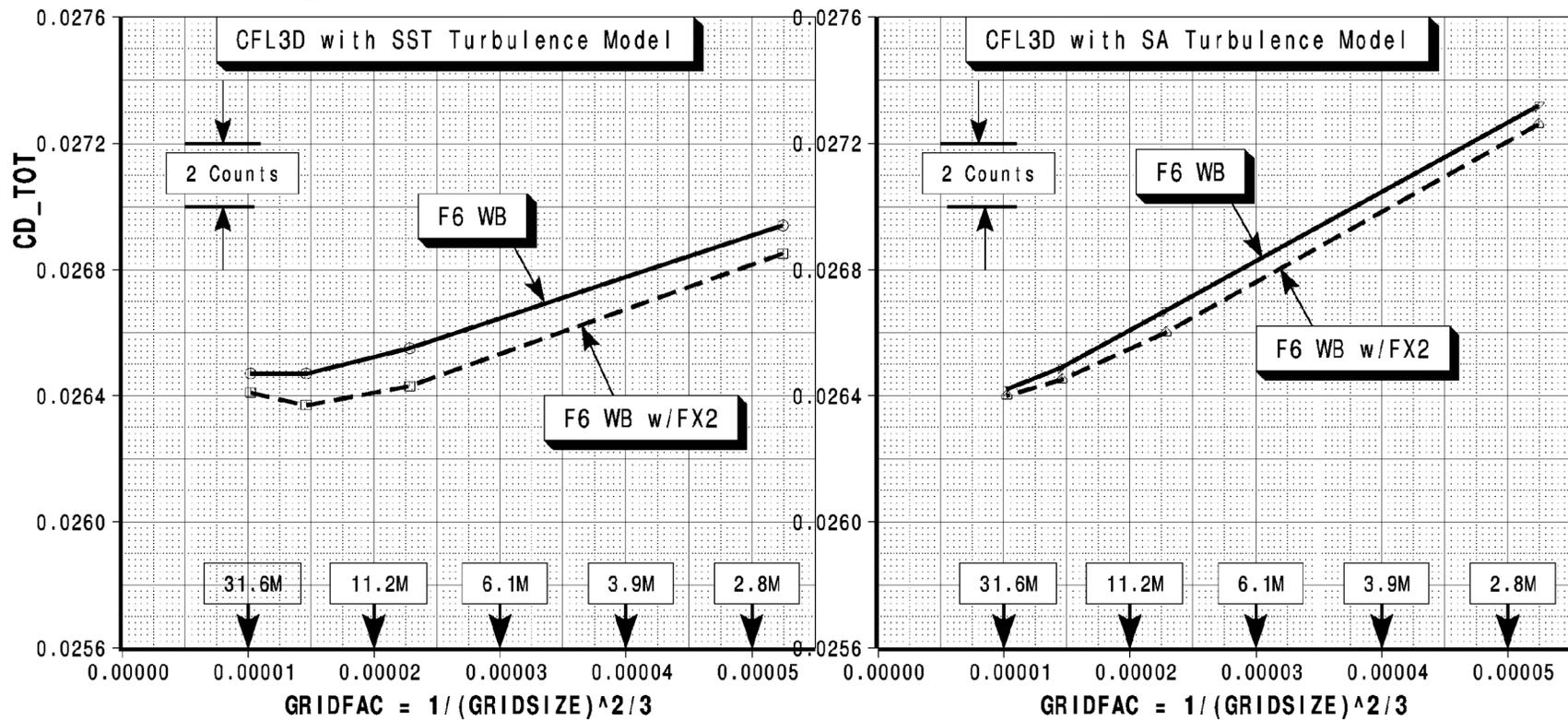
Wind Tunnel Oil Flow Photo, Re=3M



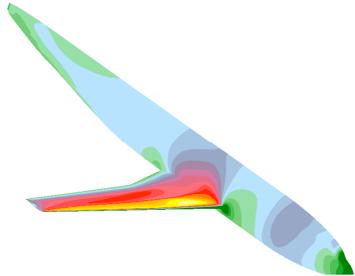
F6 WB w/wo FX2 – Total Drag Convergence



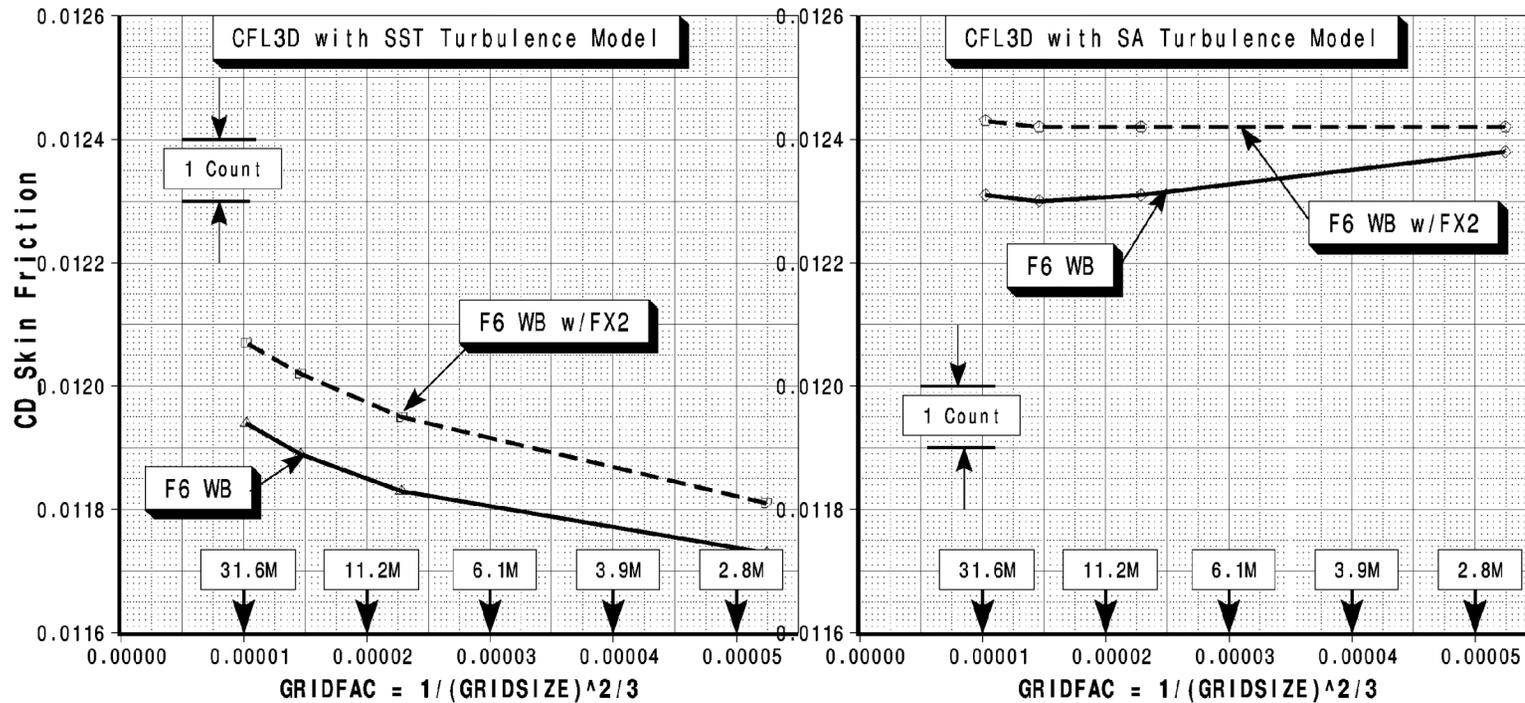
F6 Wing-Body w/wo FX2, MACH = 0.75
Re = 5 Million, Fixed CL=0.50



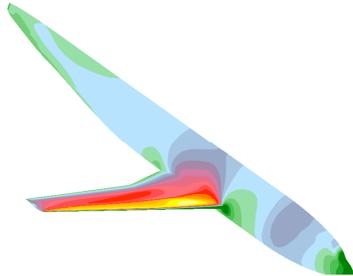
F6 WB w/wo FX2 – Skin Friction Drag Convergence



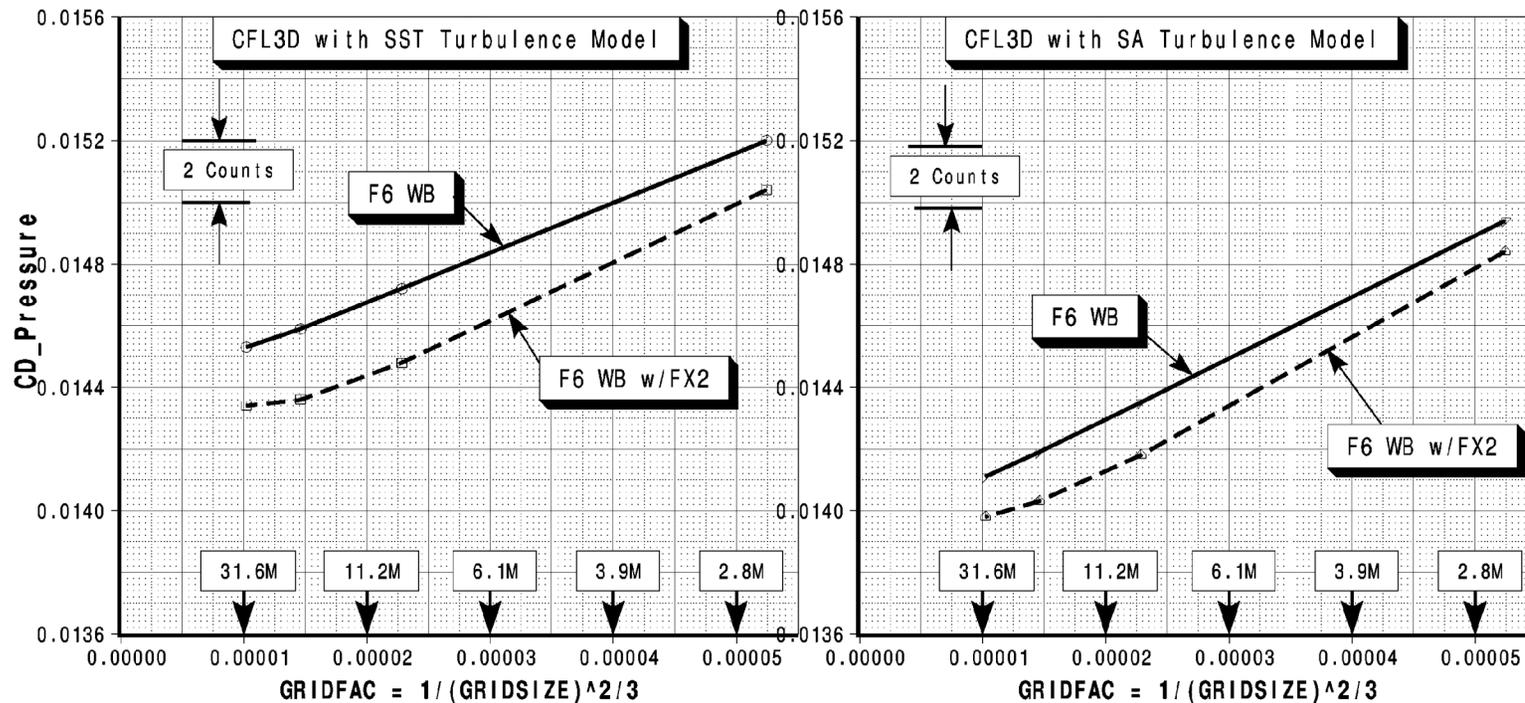
F6 Wing-Body w/wo FX2, MACH = 0.75
Re = 5 Million, Fixed CL=0.50



F6 WB w/wo FX2 – Pressure Drag Convergence

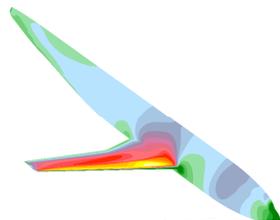


F6 Wing-Body w/wo FX2, MACH = 0.75
Re = 5 Million, Fixed CL=0.50

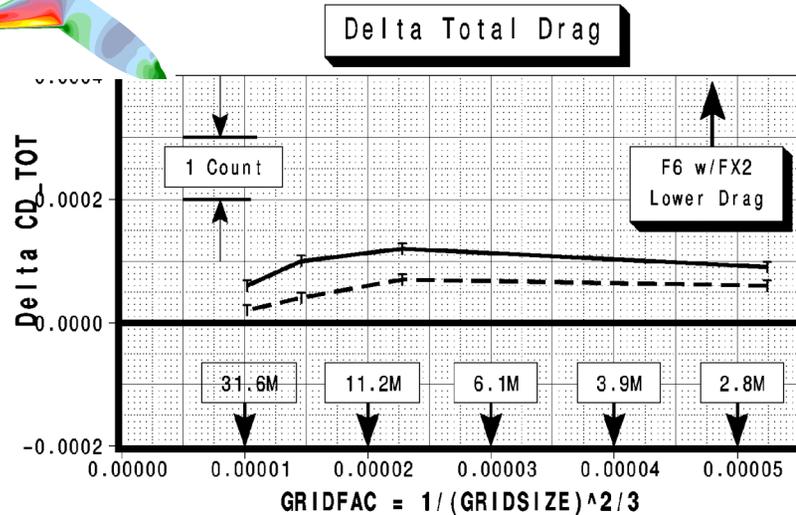


F6 WB w/wo FX2 – Drag Increment Grid Convergence

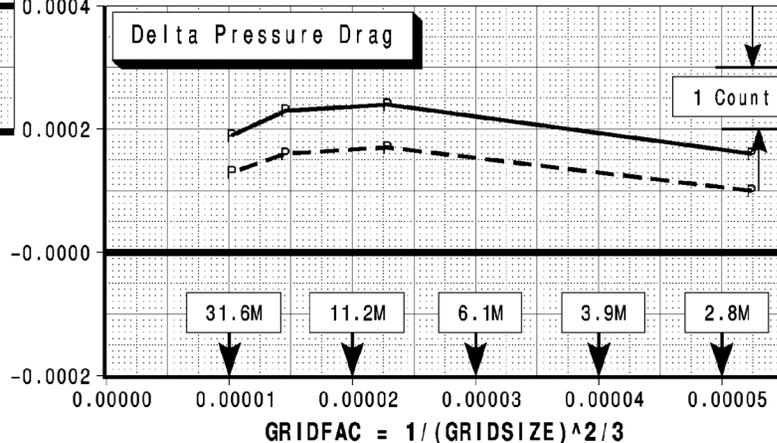
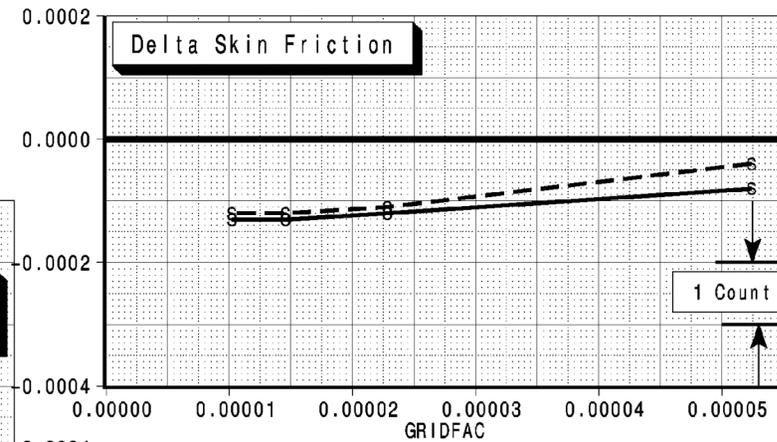
$$\Delta = (\text{F6 WB}) - (\text{F6 WB w/FX2})$$



Wing-Body w/wo FX2, MACH = 0.75
Re = 5 Million, Fixed CL=0.50



— SST Turbulence Model
- - - SA Turbulence Model

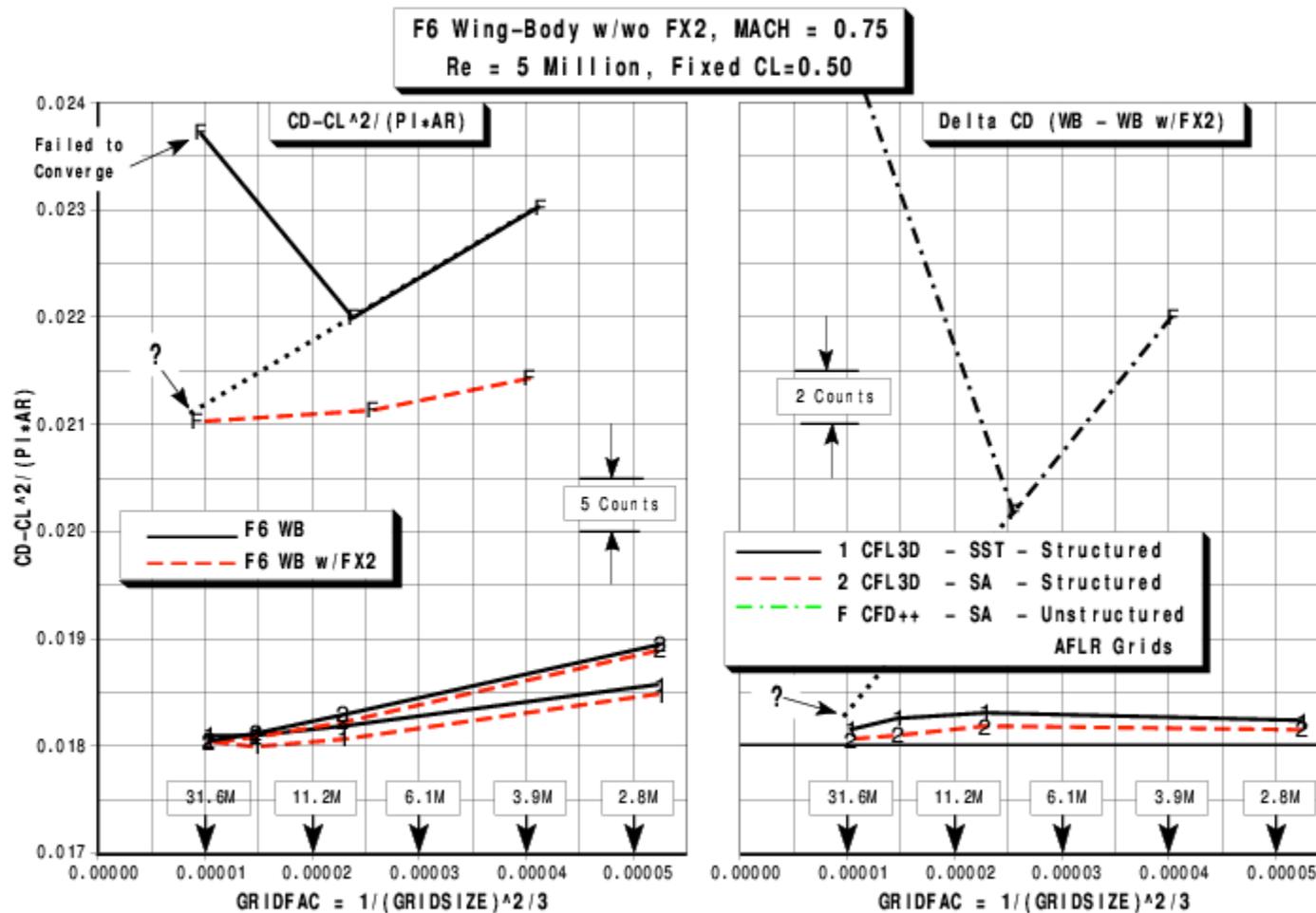




CFD++ – Unstructured Grid Navier-Stokes Code

- Developed by Metacomp Technologies
- Unified grid, unified physics and advanced numerical discretization and solution framework.
- Finite volume
- Upwind biased
- Multigrid for acceleration
- Arbitrary elements and has overset capabilities.
- Choice of turbulence models
 - Spalart-Almaras SA Model
 - $k-\varepsilon$ -Rt Model
- Time accurate with dual-time stepping
- Runs efficiently on parallel machines through MPI

CFD++ – Unstructured Grid Navier-Stokes Code Grid Convergence





Concluding Remarks

Zeus/CFL3D – Structured Grids

- Zeus/CFL3D exhibited reasonable grid convergence characteristics for both SA and SST turbulence models.
 - Good sequence of grids
 - Good solution convergence
 - Concern with trend at finest grids
- Separation bubble size little affected by grid size, some difference with turbulence model
- Pressure distributions essentially invariant with grid

CFD++ - Unstructured Grids

- F6 Wing-Body: Good temporal convergence on coarse and medium St. Louis mixed-element grids; non-convergence observed on fine St. Louis grid because of large, spurious side of body separation.
- F6 Wing-Body with FX2 Fairing: Very good temporal convergence on all St. Louis mixed-element grids. Divergence observed with Langley grids, generated using VGRID.